

1. Coordinate system

- various definition exist!

\vec{s} - particle direction
 \vec{y} - upwards
 \vec{x} - bending plane

} curvilinear system

Coordinate system is defined on the reference/nominal/sollbahn trajectory !

- metric

$$r(s) = \vec{r}_0(s) + x(s)\vec{u}_x(s) + y(s)\vec{u}_y(s)$$

$$d\vec{r} = \vec{u}_x dx + \vec{u}_y dy + \vec{u}_s (1 + hx) ds$$

$$h = \frac{1}{\rho_0} \quad \rho_0 - \text{curvature of nominal trajectory}$$

$$h(s) = \frac{1}{\rho_0(s)} = \frac{q}{p_0} B_y(x=0, y=0, s) = \frac{q}{p_0} B_0(s)$$

q, p_0 - charge and momentum of reference particle

(slide)

- deviation of a particle in 3-dimensions

 $\Delta x, \Delta y, \Delta z$ - in space $\Delta p_x, \Delta p_y, \Delta p_z$ - in momentum

} 6 parameters

$$\Delta p_x, \Delta p_y, \Delta p_z \ll p_0$$

$$x' = \frac{dx}{ds} = \frac{\Delta p_x}{p_0}, \quad y' = \frac{dy}{ds} = \frac{\Delta p_y}{p_0}, \quad l = -\delta_0(t - t_0)$$

early particle $t < t_0; l > 0$

$$\delta = \frac{p - p_0}{p_0}$$

$$\begin{matrix}
 \cancel{x(s)} \\
 \begin{pmatrix} x \\ x' \\ y \\ y' \\ l \\ \delta \end{pmatrix}
 \end{matrix}
 =
 \begin{pmatrix}
 \text{radial orbit deviation} \\
 \text{radial direction deviation} \\
 \text{axial} \quad \dots \\
 \text{axial} \quad \dots \\
 \text{longitudinal} \quad \dots \\
 \text{momentum deviation}
 \end{pmatrix}$$

Since x, x', y, y', l, δ are small \Rightarrow mm, mrad, pmrad

Equations of motion

(Linear approximation) (dipole, quadrupole magnets...)

- Lorentz force $\dot{\vec{p}} = q(\vec{v} \times \vec{B})$
 $\ddot{\vec{r}} = q(\vec{v} \times \vec{B}) / \delta m$

a) dipole magnet

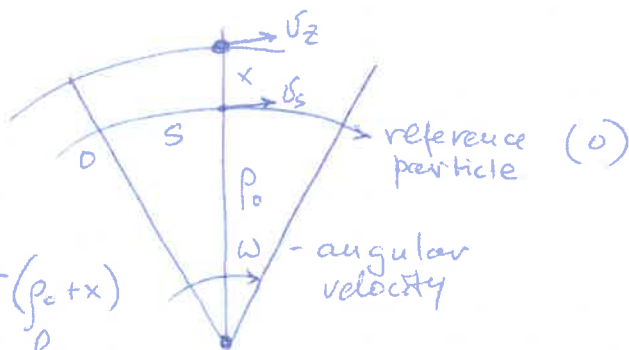
radius = $\rho = \rho_0 + x$
 velocity $v = v_z = (\rho_0 + x)\omega$

radial acceleration $a_r = -\omega^2(\rho_0 + x)$

• Lorentz force + centrifugal force

$$\ddot{x} = \ddot{x} + a_r = \ddot{x} - \omega^2(\rho_0 + x) = \frac{q}{\delta m} (v_y B_z - v_z B_y) \quad (1)$$

$$\ddot{y} = \frac{q}{\delta m} (v_z B_x - v_x B_z) \quad (2)$$



$v_x, v_y \ll v_z \rightarrow$ can neglect $v_x B_z, v_y B_z$ (we are still in linear approximation)

$$v = v_z \sqrt{1 + x^2 + y^2} \approx v_z$$

$$\rho = \delta m v \approx \delta m v_z = \delta m \rho_0 \omega (1 + x/\rho_0), \quad x/\rho_0 \ll 1 \text{ (mm vs m)}$$

• replacing $\delta m = p/v$ obtain for (1) and (2)

$$\ddot{x} - \omega^2(\rho_0 + x) = -\frac{q}{p} v_z^2 B_y \quad (3)$$

$$\ddot{y} = +\frac{q}{p} v_z^2 B_x \quad (4)$$

now: get rid of time: $\frac{ds}{dt} = \rho_0 \omega$

$$\frac{d}{dt} = \frac{ds}{dt} \frac{d}{ds} = \rho_0 \omega \frac{d}{ds}, \quad \frac{d^2}{dt^2} = (\rho_0 \omega)^2 \frac{d^2}{ds^2}$$

• divide (3) and (4) by $(\rho_0 \omega)^2$:

$$x'' - \frac{1}{\rho_0} \left(1 + \frac{x}{\rho_0}\right) = -\frac{q}{p} B_y \left(1 + \frac{x}{\rho_0}\right)^2 \quad (5)$$

$$y'' = +\frac{q}{p} B_x \left(1 + \frac{x}{\rho_0}\right)^2 \quad (6)$$

• using the definition of field index:

$$n \equiv \frac{-dB/B}{dr/r} = -\frac{r}{B} \cdot \frac{dB}{dr} \quad \text{where } r - \text{radius}$$

$$n = -\frac{\partial B_y}{\partial x} \frac{\rho_0}{B_0}$$

$$B_x = B_0 \left(0 - \frac{ny}{\rho_0}\right)$$

$$B_y = \int_{\rho_0}^{\rho_0+x} \frac{-nB_0}{\rho} dx = -\frac{nB_0}{\rho_0} \Big|_{\rho_0}^{\rho_0+x} + B_0$$

$$B_y = B_0 \left(1 - \frac{nx}{\rho_0}\right)$$

- we can now rewrite (5) and (6) -3- (24)

$$x'' = -B_0 \frac{q}{p} \left(1 - \frac{nx}{p_0}\right) \left(1 + \frac{x}{p_0}\right)^2 + \frac{1}{p_0} \left(1 + \frac{x}{p_0}\right) \quad (7)$$

$$y'' = -B_0 \frac{q}{p} \frac{ny}{p_0} \left(1 + \frac{x}{p_0}\right)^2 \quad (8)$$

- relative momentum deviation

$$\frac{1}{p} = \frac{1-\delta}{p_0}, \text{ where } p_0 = qB_0\rho_0 \quad \left(\delta = 1 - \frac{p}{p_0} \approx \frac{p-p_0}{p_0}\right)$$

$$\left. \begin{aligned} x'' + \frac{1-n}{\rho_0^2} x &= \frac{1}{\rho_0} \delta \\ y'' + \frac{n}{\rho_0^2} y &= 0 \end{aligned} \right\} (9)$$

$$\left. \begin{aligned} k_x &= \frac{1-n}{\rho_0^2} \\ k_y &= \frac{n}{\rho_0^2} \\ h &= \frac{1}{\rho_0} \end{aligned} \right\} \begin{array}{l} \text{define} \\ \leftarrow \text{curvature} \end{array}$$

$$\boxed{\begin{aligned} x'' + k_x x &= h\delta \\ y'' + k_y y &= 0 \end{aligned}} \quad (10)$$

Second-order linear ordinary differential equation = Hill
 k_y - has to be periodic

- b) Quadrupole magnet (easier, nominal orbit \rightarrow straight)

- Components of magnetic field

$$\begin{aligned} B_x &= gy & (g - \text{gradient of the field } g = \frac{\partial B_x}{\partial y} = \frac{\partial B_y}{\partial x}) \\ B_y &= gx \end{aligned}$$

$$\left. \begin{aligned} \dot{x} &= -\frac{q}{\delta m} v_z gx \\ \dot{y} &= +\frac{q}{\delta m} v_z gy \end{aligned} \right\} (11)$$

- approximations $v \approx v_z, \delta m v = p = p_0(1+\delta) \approx p_0$

$$\left. \begin{aligned} x'' + \frac{g^2}{p_0} x &= 0 \\ y'' - \frac{g^2}{p_0} y &= 0 \end{aligned} \right\} (12)$$

$$\left. \begin{aligned} k_x &= +\frac{g^2}{p_0} \\ k_y &= -\frac{g^2}{p_0} \end{aligned} \right\} \text{define}$$

$$\boxed{\begin{aligned} x'' + k_x x &= 0 \\ y'' + k_y y &= 0 \end{aligned}} \quad (13)$$

3. Solutions of equations of motion

-4- (24)

- for a reference particle, or monoenergetic particles

$$\begin{cases} x'' + K_x(s)x = 0 \\ y'' + K_y(s)y = 0 \end{cases} \quad (14)$$

- General solution

$$x(s) = x_0 C_x(s) + x'_0 S_x(s)$$

x_0, x'_0, y_0, y'_0 -

$$y(s) = y_0 C_y(s) + y'_0 S_y(s)$$

- start values

C_x, C_y (S_x, S_y) are cosine (sine) - similar solutions

$$C_x(0) = 1 \quad S_x(0) = 0$$

$$C_x'(0) = 0 \quad S_x'(0) = 1$$

and the same for y, y'

- if particles are not monoenergetic ($\delta \neq 0$) \rightarrow inhomogeneous Eq

$$x'' + K_x(s)x = h(s)\delta \quad (\text{dipole})$$

solution from homogeneous differential Eq. plus solution of inhomogeneous eq.

$$x(s) = x_0 C_x(s) + x'_0 S_x(s) + \delta dx(s)$$

\uparrow
- particular solution
- dispersion function

Particles are sorted dependent on the field index = correlation of δ and x = dispersion

$$dx(s) = \int_0^s h(\bar{s}) G_x(s, \bar{s}) d\bar{s} \quad - \text{with green function}$$

$$G_x(s, \bar{s}) = S_x(s) C_x(\bar{s}) - C_x(s) S_x(\bar{s})$$

with initial conditions $dx(0) = 0; dx'(0) = 0$

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PPT

$$x_0 = 1 \text{ mm}, \quad x'_0 = 1 \text{ mrad}, \quad \delta = 1 \text{ pramid}$$

$$y_0 = 1 \text{ mm}, \quad y'_0 = 1 \text{ mrad}$$

- Characteristic solutions for transverse motion -5 (24)
 drift, quadrupole, dipole

"Sharp cut-off" - no trapping fields, effective lengths

$K_x, K_y = \text{const}$ within $L \Rightarrow$ (14) - harmonic oscillator

	$K_x(s) > 0$ & $K_y(s) > 0$	$K_x(s) = K_y(s) = 0$	$K_x(s) < 0, K_y(s) < 0$
$C_x(s)$	$\cos(\sqrt{K_x} s)$	1	$\cosh(\sqrt{ K_x } s)$
$S_x(s)$	$\frac{1}{\sqrt{K_x}} \sin(\sqrt{K_x} s)$	s	$\frac{1}{\sqrt{ K_x }} \sin(\sqrt{ K_x } s)$
$d_x(s)$	$\frac{n}{K_x} [1 - \cos(\sqrt{K_x} s)]$	0	$\frac{n}{\sqrt{ K_x }} [-1 + \cosh(\sqrt{ K_x } s)]$
$C_y(s)$	$\cos(\sqrt{K_y} s)$	1	$\cosh(\sqrt{ K_y } s)$
$S_y(s)$	$\frac{1}{\sqrt{K_y}} \sin(\sqrt{K_y} s)$	s	$\frac{1}{\sqrt{ K_y }} \sin(\sqrt{ K_y } s)$
	oscillatory behavior		divergent

examples

quadrupole

$$K_x = -K_y \Rightarrow \text{foc/defoc}$$

solenoid

$$K_x = K_y \Rightarrow \text{foc/foc or defoc/defoc}$$

dipole

$$K_x = \frac{1-n}{\rho_0^2} \quad K_y = \frac{n}{\rho_0}$$

$$0 < n < 1 \quad \text{foc/foc}$$

$$\cosh(x) = \frac{e^x + e^{-x}}{2}$$

$$\sinh(x) = \frac{e^x - e^{-x}}{2}$$

- Characteristic solutions in the longitudinal direction
 at start: orbital deviation $l(0) = l_0$ at the end $l(s) = l$

$$l(s) - l(0) = \mathcal{R}_0(t_0 - t) \Rightarrow$$

$$\Rightarrow -x_0 \int_0^s h(\bar{s}) C_x(\bar{s}) d\bar{s} - x_0' \int_0^s h(\bar{s}) S_x(\bar{s}) d\bar{s} +$$

$$+ l_0 - \delta \left(\int_0^s h(\bar{s}) d_x(\bar{s}) d\bar{s} - \frac{s}{\rho^2} \right)$$

4. Transfermatrix

$\vec{x}(s) = R(s) \vec{x}(0)$ det $R = 1$ (Liouville's Theorem)

in linear approximation - we have decoupled planes

$$R = \begin{bmatrix} R_{11} & R_{12} & 0 & 0 & 0 & R_{16} \\ R_{21} & R_{22} & 0 & 0 & 0 & R_{26} \\ 0 & 0 & R_{33} & R_{34} & 0 & 0 \\ 0 & 0 & R_{43} & R_{44} & 0 & 0 \\ R_{51} & R_{52} & 0 & 0 & 1 & R_{56} \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

position dispersion
angle dispersion

independent description of dispersion then 3x3

$$\begin{pmatrix} x \\ x' \\ y \\ y' \\ l \\ \delta \end{pmatrix}$$

- accelerator structure $R = \prod R_i$

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$$R_x = \begin{pmatrix} R_{11} & R_{12} & R_{16} \\ R_{21} & R_{22} & R_{26} \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} C_x & S_x & dx_x' \\ C_x' & S_x' & dx_x \\ 0 & 0 & 1 \end{pmatrix}$$

a) drift

$$\begin{cases} x = x_0 + Lx_0' \\ x' = x_0' \\ y = y_0 + Ly_0' \\ y' = y_0' \\ l = l_0 + \left(\frac{L}{\beta^2}\right) \delta_0 \\ \delta = \delta_0 \end{cases}$$

$$R = \begin{bmatrix} 1 & L & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & L & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & L/\beta^2 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

b) quadrupole Slide

field strength at the pole
radius aperture

$$k = \frac{|g|}{(B\rho)_0} = \left(\frac{|B_0|}{a} \right) \frac{1}{(B\rho)_0}$$

$K_x = k, K_y = -k$ - foc

c) dipole (homogeneous)

$$K_x = \frac{1}{\rho_0^2}, K_y = 0, h = \frac{1}{\rho_0}, \alpha = \frac{L}{\rho_0}$$

↑ bending angle

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radial → foc
axial → drift

d) weak focusing dipole (cyclotron)

-7- (4)

$$0 < n < 1$$

$$n = - \frac{\partial B_y}{\partial x} \frac{\rho_0}{B_0}$$

$$K_x = \frac{1-n}{\rho_0^2}, \quad K_y = \frac{n}{\rho_0^2}, \quad h = \frac{1}{\rho_0}, \quad d = \frac{L}{\rho_0}$$

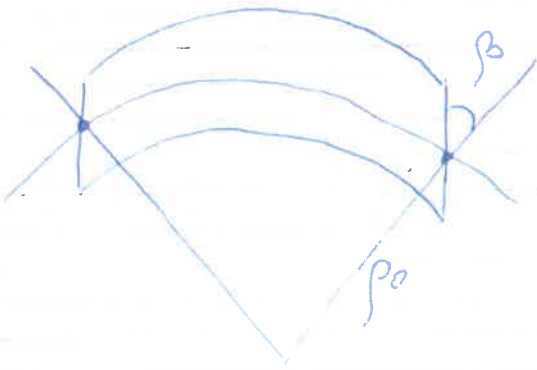
both planes focusing

e) strongly focusing dipole (synchrotron)

$$n > 0 \text{ or } n > 1 \quad |n| \approx 2$$

focus in one plane + defocus in the other

5. Edge Focusing -



$$X = X_0, \quad X' = \frac{\tan \beta}{\rho_0} X_0 + X_0'$$

$$Y = Y_0, \quad Y' = - \frac{\tan \beta}{\rho_0} Y_0 + Y_0'$$

focusing in one plane
defocusing in the other