

Ansatz:



velocity in x direction

Insertion and differentiation leads to 2 linear equations in \mathscr{Q}' and S'

frequency of wave

$$\begin{bmatrix} \left(\frac{v}{v_1}\right)^2 - 1 \end{bmatrix} \varrho' + \left(\frac{\partial p}{\partial S}\right)_{\varrho} \left(\frac{\partial \varrho}{\partial p}\right)_{S} S' = 0, \quad (i)$$

$$\left(\frac{\partial T}{\partial \varrho}\right)_{S} \left(\frac{\partial S}{\partial T}\right)_{\varrho} \varrho' + \left[\left(\frac{v}{v_2}\right)^2 - 1\right] S' = 0 \quad (ii)$$

with

$$v_1^2 = \left(\frac{\partial p}{\partial \varrho}\right)_S$$
 and $v_2^2 = \frac{\varrho_s}{\varrho_n} S^2 \left(\frac{\partial T}{\partial S}\right)_{\varrho}$





the constrains equation for the coefficients is

$$\left[\left(\frac{v}{v_1}\right)^2 - 1 \right] \left[\left(\frac{v}{v_2}\right)^2 - 1 \right] = \left(\frac{\partial p}{\partial S}\right)_{\varrho} \left(\frac{\partial \varrho}{\partial p}\right)_{S} \left(\frac{\partial T}{\partial \varrho}\right)_{S} \left(\frac{\partial S}{\partial T}\right)_{\varrho} \right]$$
here standard thermodynamic relations are used
$$\left[\left(\frac{v}{v_1}\right)^2 - 1 \right] \left[\left(\frac{v}{v_2}\right)^2 - 1 \right] = \frac{C_p - C_V}{C_p}$$

for liquid helium $C_p \approx C_V$

$$\left[\left(\frac{v}{v_1} \right)^2 - 1 \right] \left[\left(\frac{v}{v_2} \right)^2 - 1 \right] \approx 0$$
 (iii)

interpretation: two wave

$$\left\{ \begin{array}{c} v_1 \\ v_2 \end{array} \right\}$$
 weakly coupled

via $\frac{C_p - C_V}{C_p}$





(i) First sound

with (i) and (iii)

$$v = v_1 = \sqrt{\left(\frac{\partial p}{\partial \varrho}\right)_S}$$

 $\left(\frac{v}{v_1}\right)^2 - 1 = 0$

$$\varrho' \neq 0$$
 $S' = 0$
 \downarrow $grad T = 0$
 \uparrow

as usual for ordinary (first) sound

insert (4) into (6)

$$\varrho_{n} \frac{\partial}{\partial t} (\mathbf{v}_{n} - \mathbf{v}_{s}) = \varrho S \operatorname{grad} T = 0$$

$$\mathbf{v}_{n} = \mathbf{v}_{s} \longrightarrow \operatorname{superfluid} \operatorname{and} \operatorname{normalfluid} \operatorname{component} \operatorname{are} \operatorname{in} \operatorname{phase}$$

$$(4) in (6)$$

$$\frac{\partial \overline{v}_{s}}{\partial t} = S \operatorname{grad} T + \frac{1}{S} \frac{\partial \overline{J}}{\partial t}$$
insert (2) ×S
$$\frac{\partial (\overline{v}_{s})}{\partial t} = S \operatorname{grad} T + S_{n} \frac{\partial \overline{v}_{n}}{\partial t} + S_{s} \frac{\partial \overline{v}_{s}}{\partial t}$$

$$\frac{\partial (\overline{v}_{s})}{\partial t} = S \operatorname{grad} T + S_{n} \frac{\partial \overline{v}_{n}}{\partial t} + S_{s} \frac{\partial \overline{v}_{s}}{\partial t}$$

$$\frac{\partial (\overline{v}_{s} - \overline{v}_{n})}{\partial t} = S \operatorname{grad} T = 0$$



(i) First sound

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• for
$$T \rightarrow 0$$
: $v_1 \approx 238 \,\mathrm{m \, s^{-1}}$.

only density variation \implies almost ordinary sound

▶ for $T \to T_{\lambda}$: corrections become important



2.3 Properties of He-II described using the two-fluid model

(ii) Second sound

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 $\sqrt{2}$

with (ii) and (iii) we find

$$v = v_2 = \sqrt{\frac{\varrho_{\rm s}}{\varrho_{\rm n}}} S^2 \left(\frac{\partial T}{\partial S}\right)_{\!\varrho}$$

$$\left(\frac{v}{v_2}\right) - 1 = 0$$
 $S' \neq 0$, $\varrho' = 0$
 \downarrow grad $p = 0$

with (4)

$$\frac{\partial \boldsymbol{j}}{\partial t} = -\operatorname{grad} p \stackrel{!}{=} 0 \quad \longrightarrow \quad \frac{\partial \varrho_{\mathrm{n}} \boldsymbol{v}_{\mathrm{n}}}{\partial t} + \frac{\partial \varrho_{\mathrm{s}} \boldsymbol{v}_{\mathrm{s}}}{\partial t} = 0$$

 $\varrho_{\rm n} \boldsymbol{v}_{\rm n} + \varrho_{\rm s} \boldsymbol{v}_{\rm s} = 0$

no mass flow in closed vessel

 $\bigcirc \ \varrho_n \uparrow$, $\varrho_s \downarrow$ counter flow and no density variation

temperature wave





ultra-low temperatures:

excitations at $T \rightarrow 0$ are only longitudinal phonons Landau

 $A = 2\pi^2 k_{\rm B}^4 / (45\hbar^3 v_1^3 \varrho)$

Debye model

$$C_p = 3AT^3$$
$$S = AT^3$$

in addition

 ϱ

$$\begin{array}{c}
\varrho_{\rm s} \approx \varrho \\
\varrho_{\rm n} = A \varrho T^4 / v_1^2
\end{array} \quad \text{for } T \to 0: \\
v_2 \to v_1 / \sqrt{3} \approx 137 \,\mathrm{m \, s^{-1}}
\end{array}$$







3rd sound experiment

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Procedure

- periodic local heating
- $\blacktriangleright Q_s$ flows to warm location \blacksquare thickness changes
- ► surface wave \triangleq 3rd sound
- optical detection of thickness



Measurement and results

- ► 3rd sound velocity vs. *z* (log/log plot)
- different surfaces: v_3 almost independent
- line rightarrow theory $v_3 \propto \sqrt{z}$
- good agreement except for very thick films

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3rd sound experiment: temperature dependence



Measurement and results

- 3^{rd} sound velocity vs T
- points at T = 1.25 K normalized to (•)
- v_3 is rising with decreasing T
- ▶ $T \rightarrow 0$: $v_3 = 1.5 \text{ m/s}$ (very slow)
- dashed line m riangle theory $v_3 \propto \sqrt{arrho_{
 m s}}$
- systematic deviations: origin unknow, but likely due to generation process

3rd sound in very thin films:

3rd sound propagation can be observed down to 2.1 monolayers

onset of superfluidity

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2.3 Properties of He-II described using the two-fluid model

3rd sound in moving films:





Detection of 3rd sound experiment in ultralow films:

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time



Experimental results:



for ultrathin films:

$$v_3^2 = \frac{\overline{\rho_{\rm s}}}{\rho_{\rm s,bulk}} \frac{3RT}{m} \ln \frac{p_0}{p}$$

- experimental threshold of 2.1 monolayers independent of substrate
- film thickness determine by amount of helium and surface area
- extrapolation suggests that 1.47 monolayers might be the onset threshold





(iv) Fourth sound

sound propagation in fine powders / slits $\,oldsymbol{v}_{
m n}pprox 0$

oscillations in total density, in ratio of superfluid to normalfluid density, in pressure, in temperature, in entropy

$$v_4^2 = \frac{\varrho_{\rm s}}{\varrho} v_1^2 \left[1 + \frac{2ST}{\varrho C_p} \left(\frac{\partial \varrho}{\partial T} \right)_p \right] + \frac{\varrho_{\rm n}}{\varrho} v_2^2$$

$$\ll 1$$

$$v_{4} \approx \sqrt{\frac{\varrho_{s}}{\varrho}} v_{1}^{2} + \underbrace{\frac{\varrho_{n}}{\varrho}}_{2} v_{2}^{2} \approx \sqrt{\frac{\varrho_{s}}{\varrho}} v_{1}^{2}$$
5th sound

4th sound generation like for 1st sound, but $\boldsymbol{v}_{\mathrm{n}} pprox 0$



4th sound experiments

4th sound generation like for 1st sound, but $\boldsymbol{v}_{n} \approx 0$ $T \rightarrow 0$ $v_{4} = v_{1} \approx 238 \text{ m/s}$, since $\varrho_{s} = \varrho$ $T = T_{\lambda}$ $v_{4} = 0$

$$v_4 \approx \sqrt{\frac{\varrho_{\rm s}}{\varrho} v_1^2 + \frac{\varrho_{\rm n}}{\varrho} v_2^2}$$

Persistent flow and 4th sound

 $v_{\rm D}$

persistent flow velocity

 $v_4 \approx v_{4,0} \pm \frac{\varrho_{\rm s}}{\varrho} v_{\rm D}$

coupling of a compression wave to second sound