



Momentum of heat flow

Heat flow in He-II \longrightarrow **momentum flow** $\rho \mathbf{v} \cdot \mathbf{v}$

momentum flow / volume

resulting pressure acting on a heat source

$$p = \rho_n v_n^2 + \rho_s v_s^2 \quad (*)$$

no net mass transport (closed vessel)

$$\rho_n v_n + \rho_s v_s = 0 \quad \longrightarrow \quad v_s = -\frac{\rho_n}{\rho_s} v_n$$

insert in (*) \longrightarrow $p = \frac{\rho_n \rho}{\rho_s} v_n^2$

with heat flow / per area $\frac{\dot{Q}}{A} = \rho S T v_n \quad \xrightarrow{\frac{\dot{V}_n}{A}} \quad v_n = \frac{\dot{Q}}{A \rho S T}$



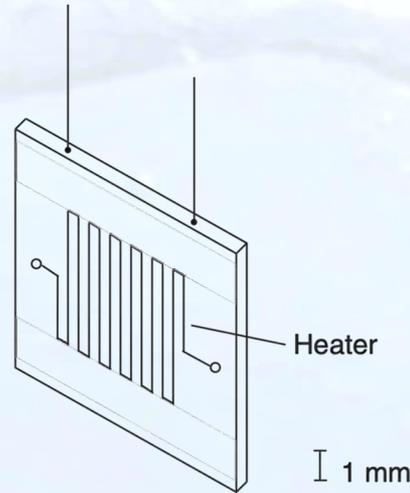
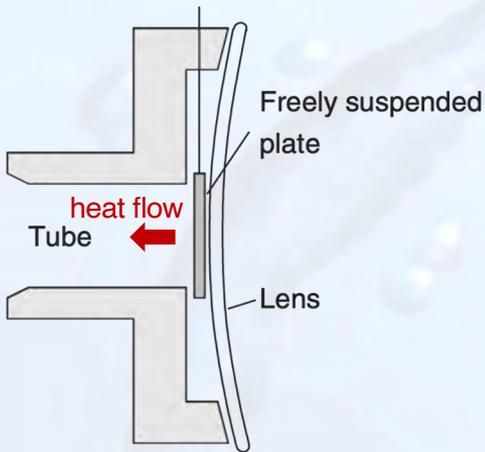
$$p = \frac{\rho_n}{\rho_s \rho} \left(\frac{\dot{Q}}{A S T} \right)^2$$

pressure associated with uni-directional **heat flow**

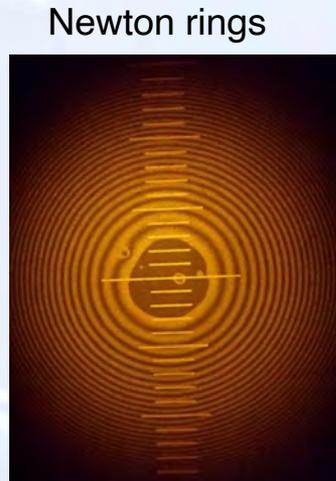
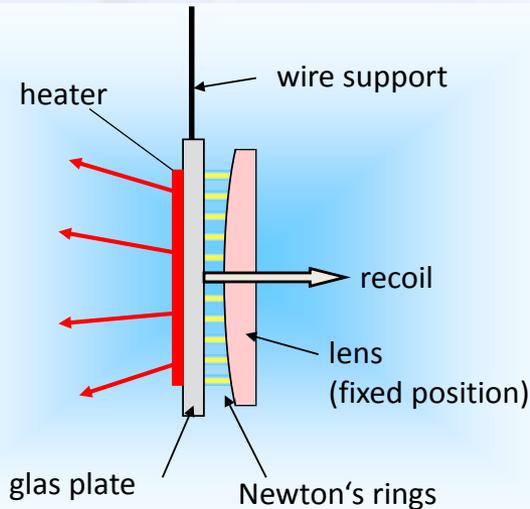
$$\begin{aligned} p &= \rho_n v_n^2 + \rho_s v_s^2 \\ &= \rho_n v_n^2 + \rho_s \left(-\frac{\rho_n}{\rho_s} v_n \right)^2 \\ &= \rho_n v_n^2 \left(1 + \frac{\rho_s}{\rho_s} \right) \\ &= \rho_n v_n^2 \left(\frac{\rho_s + \rho_n}{\rho_s} \right) \\ &= \frac{\rho_n \rho}{\rho_s} v_n^2 \end{aligned}$$



Momentum of heat flow: Measurement



change of distance between glass plate and lens measured by Newton rings → force



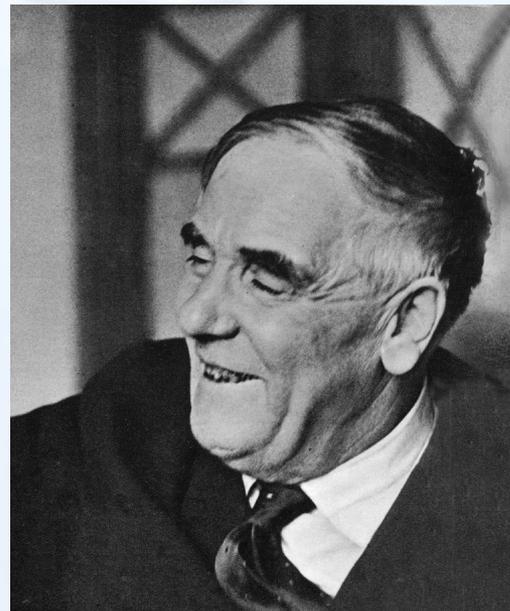
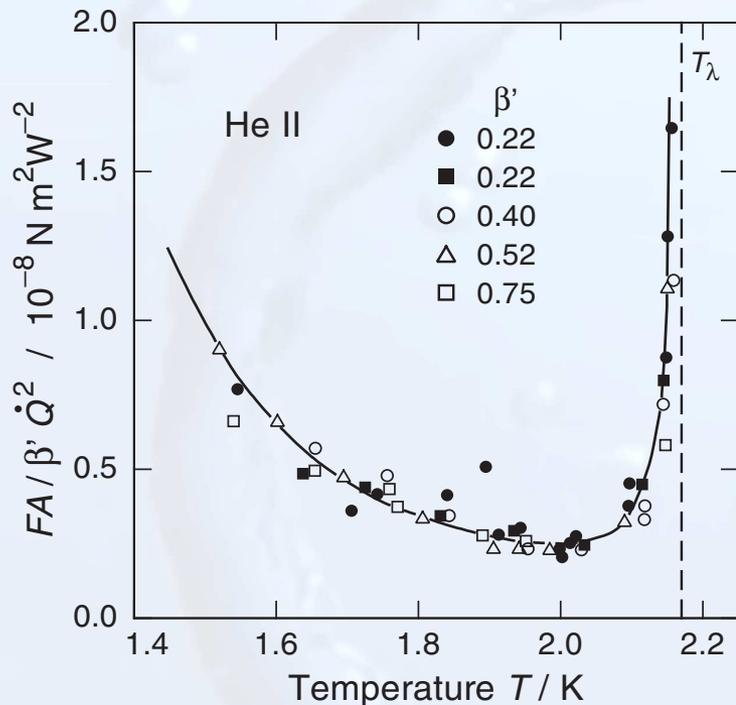
Expected force

$$F = pA = \beta' \frac{\rho_n}{\rho_s \rho A} \left(\frac{\dot{Q}}{ST} \right)^2$$

geometry dependent factor of the order of one



Momentum of heat flow: results plotted as $\frac{FA}{\beta' \dot{Q}^2} = \frac{\varrho_n}{\varrho_s \varrho} \frac{1}{T^2 S^2}$



Pyotr Leonidovich Kapitsa (1894 – 1984)

- ▶ results are **independent** of geometry
- ▶ because of $\varrho_n v_n + \varrho_s v_s = 0$ \rightarrow **rise** at **low** and **high** T
- ▶ line: **two-fluid model** (without free parameter)



density $\rho = \rho_n + \rho_s$ (1)

mass flow $\mathbf{j} = \rho_n \mathbf{v}_n + \rho_s \mathbf{v}_s$ (2)

mass conservation
continuity eqn. $\frac{\partial \rho}{\partial t} = -\text{div } \mathbf{j}$ (3)

ideal fluid $\frac{\partial \mathbf{j}}{\partial t} = -\text{grad } p$ (4)

entropy conservation $\frac{\partial(\rho S)}{\partial t} = -\text{div}(\rho S \mathbf{v}_n)$ (5)

an equation of motion for
superfluid component $\frac{\partial \mathbf{v}_s}{\partial t} = S \text{ grad } T - \frac{1}{\rho} \text{ grad } p$ (6)



d) Sound propagation (precision test of two-fluid model)

differentiation of (3) in respect to time and insert in (4)

$$\frac{\partial^2 \varrho}{\partial t^2} = \nabla^2 p \quad (*)$$

eliminate \mathbf{v}_s and \mathbf{v}_n in (5) and (6) with (2)



since not observable

neglect terms of 2nd order

$$\frac{\partial^2 S}{\partial t^2} = \frac{\varrho_s S^2}{\varrho_n} \nabla^2 T \quad (**)$$

with (*) and (**) one can **fully describe** the **sound propagation** in He-II (under the assumption we made)

$$\frac{\partial \varrho}{\partial t} = -\text{div} \vec{J} \quad (3)$$

$$\frac{\partial^2 \varrho}{\partial t^2} = -\text{div} \left(\frac{\partial \vec{J}}{\partial t} \right)$$

$$\frac{\partial \vec{J}}{\partial t} = -\text{grad } p \quad (4)$$

$$\frac{\partial^2 \varrho}{\partial t^2} = -\text{div}(-\text{grad } p)$$

$$\frac{\partial^2 \varrho}{\partial t^2} = \nabla^2 p$$



we have **2 equations**, but **4 variables** (ρ, S, p, T) however, **only 2 independent variables**

We **choose** ρ, S as **independent** and express p, T with ρ and S (for small changes)

$$\left. \begin{aligned} \delta p &= \left(\frac{\partial p}{\partial \rho} \right)_S \delta \rho + \left(\frac{\partial p}{\partial S} \right)_\rho \delta S, \\ \delta T &= \left(\frac{\partial T}{\partial \rho} \right)_S \delta \rho + \left(\frac{\partial T}{\partial S} \right)_\rho \delta S \end{aligned} \right\} \text{insert in (*) and (**)}$$



$$\frac{\partial^2 \rho}{\partial t^2} = \left(\frac{\partial p}{\partial \rho} \right)_S \nabla^2 \rho + \left(\frac{\partial p}{\partial S} \right)_\rho \nabla^2 S$$

$$\frac{\partial^2 S}{\partial t^2} = \frac{\rho_s}{\rho_n} S^2 \left[\left(\frac{\partial T}{\partial \rho} \right)_S \nabla^2 \rho + \left(\frac{\partial T}{\partial S} \right)_\rho \nabla^2 S \right]$$

2 partial differential equations of **2nd order**



Ansatz: $\varrho = \varrho_0 + \varrho' e^{i\omega(t-x/v)}$,

$$S = S_0 + S' e^{i\omega(t-x/v)}$$

frequency of wave
velocity in x direction

Insertion and differentiation leads to 2 linear equations in ϱ' and S'

$$\left[\left(\frac{v}{v_1} \right)^2 - 1 \right] \varrho' + \left(\frac{\partial p}{\partial S} \right)_\varrho \left(\frac{\partial \varrho}{\partial p} \right)_S S' = 0, \quad \text{(i)}$$

$$\left(\frac{\partial T}{\partial \varrho} \right)_S \left(\frac{\partial S}{\partial T} \right)_\varrho \varrho' + \left[\left(\frac{v}{v_2} \right)^2 - 1 \right] S' = 0 \quad \text{(ii)}$$

with

$$v_1^2 = \left(\frac{\partial p}{\partial \varrho} \right)_S \quad \text{and} \quad v_2^2 = \frac{\varrho_s}{\varrho_n} S^2 \left(\frac{\partial T}{\partial S} \right)_\varrho$$



the constrains equation for the coefficients is

$$\left[\left(\frac{v}{v_1} \right)^2 - 1 \right] \left[\left(\frac{v}{v_2} \right)^2 - 1 \right] = \underbrace{\left(\frac{\partial p}{\partial S} \right)_\rho \left(\frac{\partial \rho}{\partial p} \right)_S \left(\frac{\partial T}{\partial \rho} \right)_S \left(\frac{\partial S}{\partial T} \right)_\rho}_{\text{here standard thermodynamic relations are used}}$$

here standard thermodynamic relations are used

$$\left[\left(\frac{v}{v_1} \right)^2 - 1 \right] \left[\left(\frac{v}{v_2} \right)^2 - 1 \right] = \frac{C_p - C_V}{C_p}$$

for liquid helium $C_p \approx C_V$

$$\left[\left(\frac{v}{v_1} \right)^2 - 1 \right] \left[\left(\frac{v}{v_2} \right)^2 - 1 \right] \approx 0 \quad \text{(iii)}$$

interpretation: **two** wave $\left. \begin{matrix} \nearrow v_1 \\ \searrow v_2 \end{matrix} \right\}$ **weakly coupled** via $\frac{C_p - C_V}{C_p}$



(i) First sound

with (i) and (iii)

$$v = v_1 = \sqrt{\left(\frac{\partial p}{\partial \rho}\right)_S}$$

$$\left(\frac{v}{v_1}\right)^2 - 1 = 0$$

$$\rho' \neq 0 \quad S' = 0$$

$$\text{grad } T = 0$$

as usual for **ordinary** (first) **sound**

insert (4) into (6)

$$\rho_n \frac{\partial}{\partial t} (\underbrace{v_n - v_s}) = \rho S \text{ grad } T = 0$$

$v_n = v_s$ \rightarrow superfluid and normalfluid component are **in phase**

(4) in (6)

$$\frac{\partial \vec{v}_s}{\partial t} = S \text{ grad } T + \frac{1}{S} \frac{\partial \vec{j}}{\partial t}$$

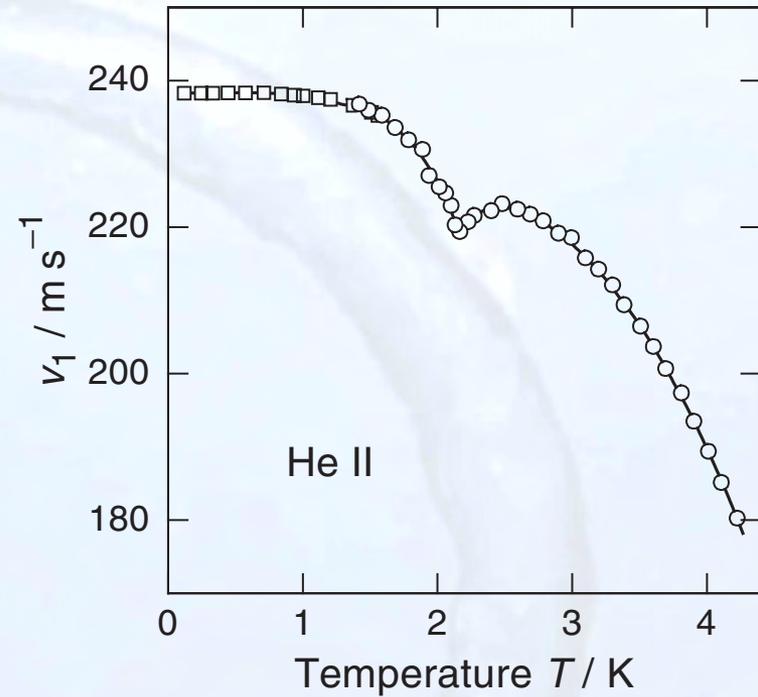
insert (2) $\times S$

$$\rho \left(\frac{\partial \vec{v}_s}{\partial t} \right) = \rho S \text{ grad } T + \rho_n \frac{\partial \vec{v}_n}{\partial t} + \rho_s \frac{\partial \vec{v}_s}{\partial t}$$

$$\rho_n \frac{\partial}{\partial t} (\vec{v}_s - \vec{v}_n) = \rho S \text{ grad } T - 0$$



(i) First sound



- ▶ for $T \rightarrow 0$: $v_1 \approx 238 \text{ m s}^{-1}$.
 ➔ only **density variation** ➔ almost **ordinary sound**
- ▶ for $T \rightarrow T_\lambda$: corrections become important



(ii) Second sound

with (ii) and (iii) we find

$$v = v_2 = \sqrt{\frac{\rho_s}{\rho_n} S^2 \left(\frac{\partial T}{\partial S} \right)_\rho}$$

$$\left(\frac{v}{v_2} \right)^2 - 1 = 0 \quad S' \neq 0, \quad \rho' = 0$$

└─ grad $p = 0$

with (4)

$$\frac{\partial j}{\partial t} = -\text{grad } p \stackrel{!}{=} 0 \quad \rightarrow \quad \frac{\partial \rho_n v_n}{\partial t} + \frac{\partial \rho_s v_s}{\partial t} = 0$$

$$\rho_n v_n + \rho_s v_s = 0$$

no mass flow in closed vessel

$\rho_n \uparrow, \rho_s \downarrow$ counter flow and no density variation

temperature wave



$$v_2 = \sqrt{\frac{\rho_s}{\rho_n} S^2 \left(\frac{\partial T}{\partial S} \right)_\rho} = \sqrt{\frac{\rho_s}{\rho_n} \frac{T S^2}{C_p}}$$

possibility to determine ρ_s/ρ_n density variation in phonon gas

ultra-low temperatures:

excitations at $T \rightarrow 0$ are **only longitudinal phonons**

Landau

Debye model

$$A = 2\pi^2 k_B^4 / (45 \hbar^3 v_1^3 \rho)$$

$$C_p = 3AT^3$$

$$S = AT^3$$

in addition

$$\rho_s \approx \rho$$

$$\rho_n = A\rho T^4 / v_1^2$$

for $T \rightarrow 0$:

$$v_2 \rightarrow v_1 / \sqrt{3} \approx 137 \text{ m s}^{-1}$$

for $T \rightarrow 0$ second sound difficult to determine since $\rho_n \rightarrow 0$

