



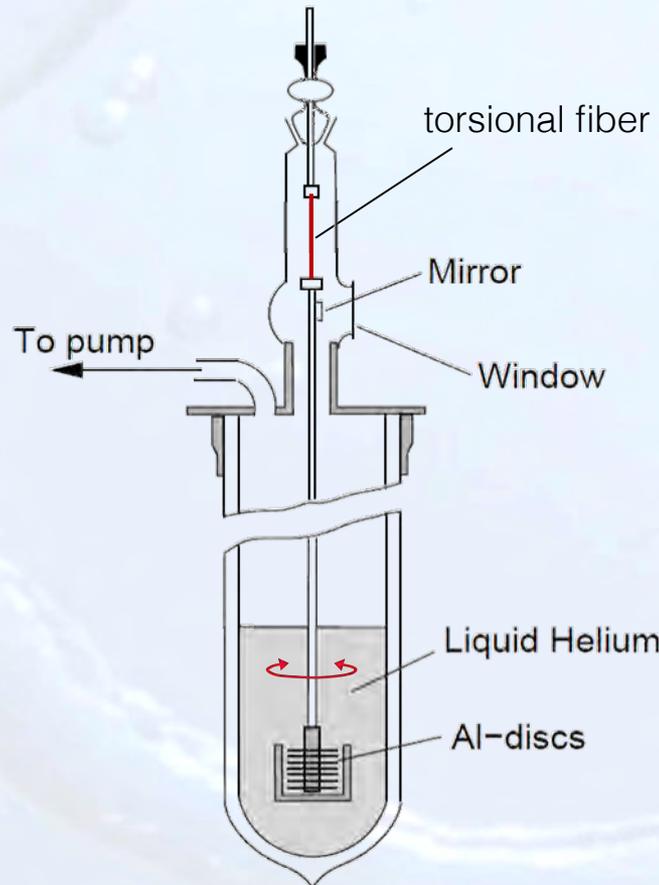
Determination of ρ_n

Experiment of Andronikasvili (1948)

First **direct** observation of ρ_n



Elepter Luarsabovich
Andronikashvili (1910-1989)



50 aluminum discs

thickness 13 μm

diameter 3.5 cm

spacing 210 μm

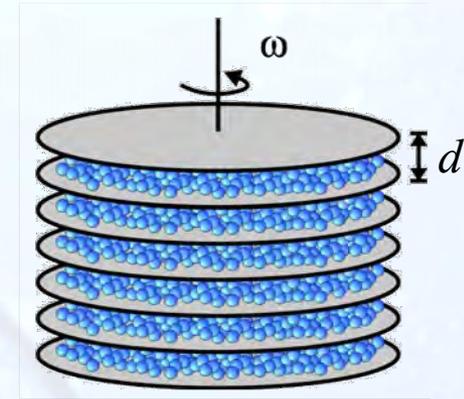


observation \rightarrow slow resonant oscillations (mass and torsion fiber)

Important parameter is the viscos penetration depth for wave with frequency ω

$$\delta = \sqrt{2\eta_n / \rho_n \omega}$$

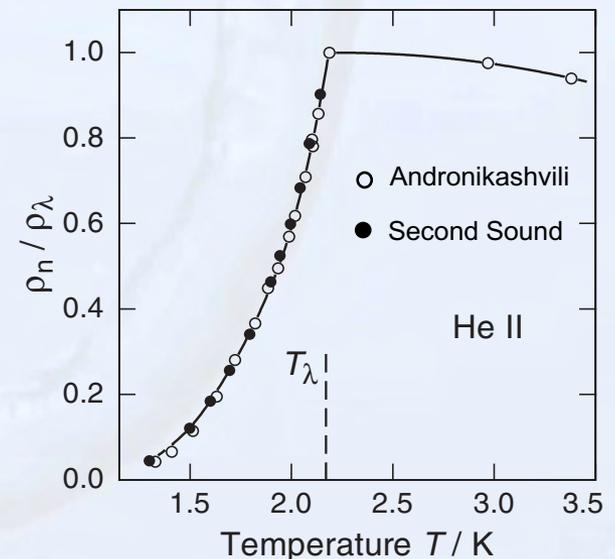
- $d < \delta$:
- \blacktriangleright ρ_n is dragged along with torsion oscillator above and below T_λ
 - \blacktriangleright ρ_s remains stationary
 - \blacktriangleright period of oscillation determined by mass of torsion oscillator (and spring constant)
- \rightarrow ρ_n can be determined



temperature dependence (empirical relation)

$$\rho_n = \rho_\lambda \left(\frac{T}{T_\lambda} \right)^{5.6}$$

comparison with 2nd Sound \rightarrow fits well





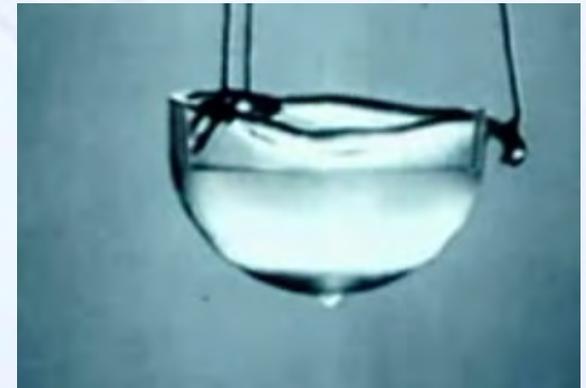
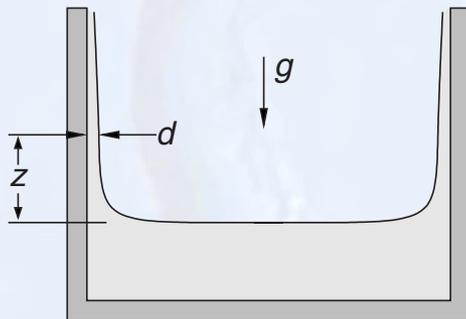
b) Beaker experiments

films are formed with a **thickness** of $\sim 200 \text{ \AA}$ in saturated vapor pressure also **against gravity**

let us understand how

comment: the film formation is a “classical” phenomenon

(i) Film formation in saturated vapor



In thermal equilibrium

$$\mu_f = \mu_g = \mu_l$$

↙ chemical potential for film (gas and liquid)

gravitational force is compensated by v. Waals forces

$$\rightarrow \mu_f = \mu_l + \underbrace{\mu_{\text{grav}} + \mu_{\text{vdW}}}_{=0} = \mu_l$$



film thickness:

$$\mu_{\text{grav}} = gz$$

$$\mu_{\text{vdW}} = -\alpha/d^3$$

$$\left. \begin{array}{l} \mu_{\text{grav}} = gz \\ \mu_{\text{vdW}} = -\alpha/d^3 \end{array} \right\} gz - \alpha/d^3 = 0 \quad \curvearrowright$$

$$d = \sqrt[3]{\frac{\alpha}{gz}}$$

depends on film thickness: $\mu_{\text{vdW}} = -\alpha/d^3$ for $d < 30 \text{ nm}$

$\mu_{\text{vdW}} = -\alpha/d^4$ for $d > 80 \text{ nm}$

atomic polarisability of helium + wall
(Hamaker constant)

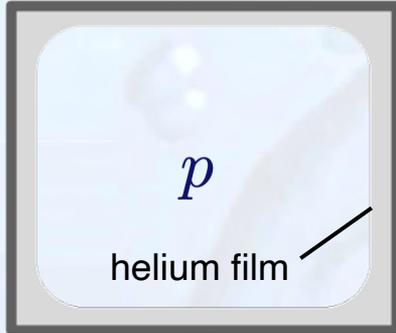
retardation of potential

typical value: $d \sim 20 \text{ nm}$ at $z = 10 \text{ cm}$

comment: property of **superfluidity** is **unimportant** for the **film formation** and **thickness**, but for the film flow



(ii) film formation in unsaturated vapor



How does d depend on p ?

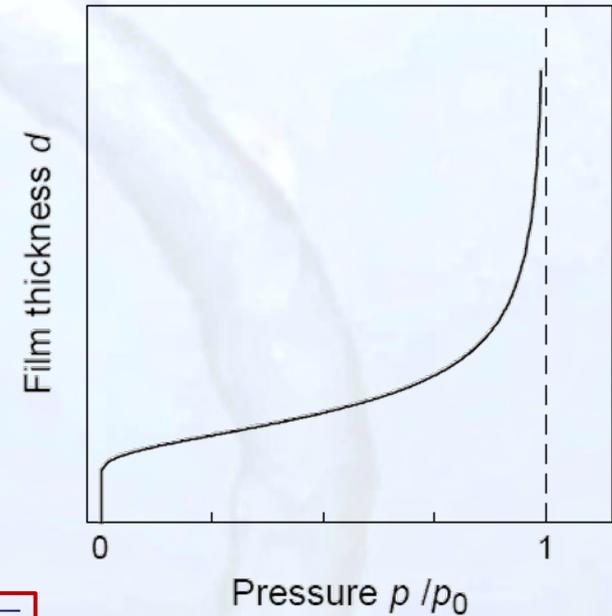
→ barometric formula

$$\frac{p}{p_0} = e^{-mgh/k_B T}$$

$$mgh = k_B T \ln \left(\frac{p}{p_0} \right)$$

→
$$\frac{\alpha}{d^3} = \frac{k_B T}{m_4} \ln \left(\frac{p_0}{p} \right)$$

→
$$d = \sqrt[3]{\frac{\alpha m_4}{k_B T (\ln p_0 - \ln p)}}$$



- ▶ decrease of pressure → decrease of film thickness
- ▶ in practice: thinknesses of **sub-mono layers** are possible and realized

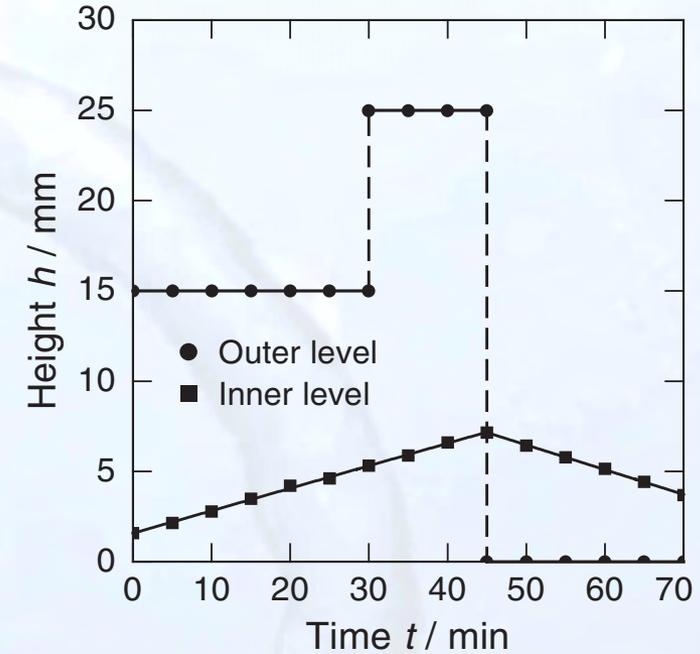


investigation of superfluidity with **third sound**: **onset of superfluidity** at $n > 2.1$ layers



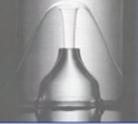
now back to the film flow:

- ▶ films are formed
- ▶ ρ_s is moving without friction
- ▶ equalizing the chemical potential is driving force
- ▶ const. rate \triangleq critical velocity



Interesting question: ρ_s flows with $S = 0$! \rightarrow rest should warm up and helium flowing into a vessel should have $T = 0$!

but thermal equilibrium via gas phase



density $\rho = \rho_n + \rho_s$ (1)

mass flow $\mathbf{j} = \rho_n \mathbf{v}_n + \rho_s \mathbf{v}_s$ (2)

mass conservation
continuity eqn. $\frac{\partial \rho}{\partial t} = -\text{div } \mathbf{j}$ (3)

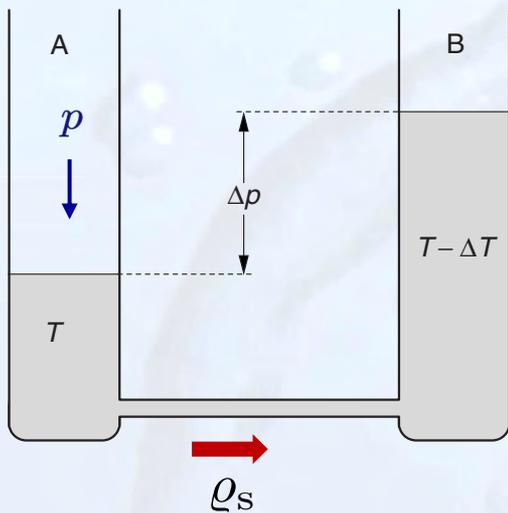
ideal fluid $\frac{\partial \mathbf{j}}{\partial t} = -\text{grad } p$ (4)

entropy conservation $\frac{\partial(\rho S)}{\partial t} = -\text{div}(\rho S \mathbf{v}_n)$ (5)

an equation of motion for
superfluid component $\frac{\partial \mathbf{v}_s}{\partial t} = S \text{ grad } T - \frac{1}{\rho} \text{ grad } p$ (6)

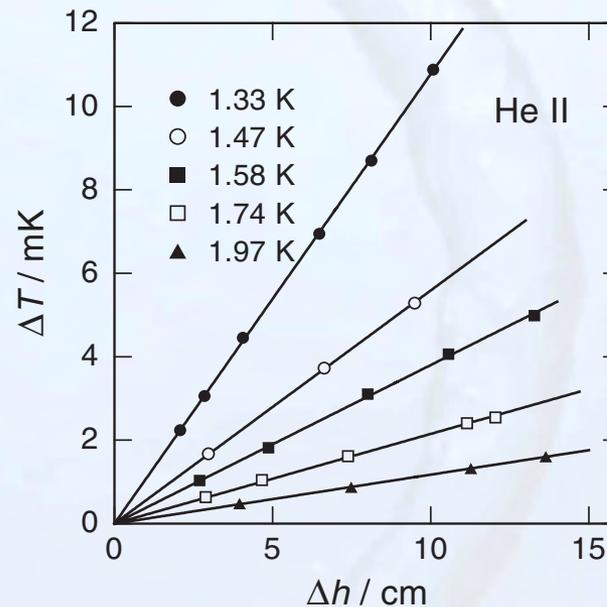


c) Thermomechanical effect



$+ Q_s \rightarrow$ cooling in B
 $- Q_s \rightarrow$ warming in A

$T_B < T_A$



Using (6) in stationary state

$$\frac{\partial v_s}{\partial t} = S \text{grad } T - \frac{1}{\rho} \text{grad } p = 0$$

↑
in equilibrium **nothing flows**

$$\frac{\Delta p}{\Delta T} = \rho S$$

London equation
(H. London 1939)

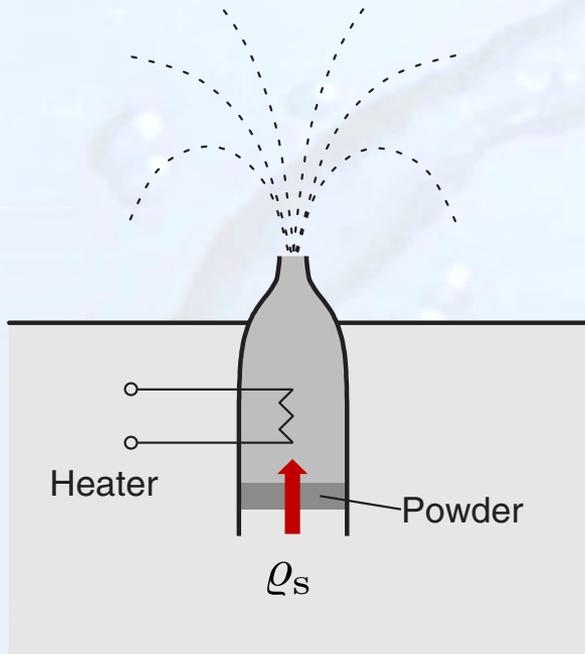
\rightarrow Linear relation between Δp and ΔT

$\Delta h = 2 \text{ cm}$
 $T = 1.5 \text{ K}$

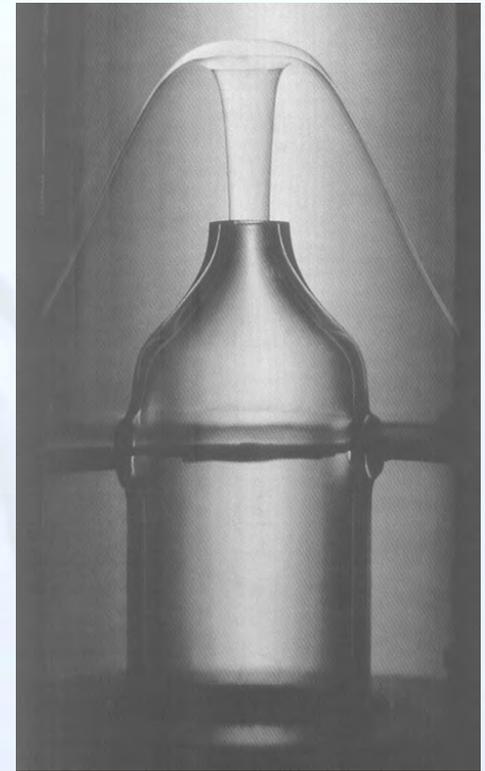
$\Delta T = 1 \text{ mK}$ not very effective cooling



Reverse thermomechanical effect: Fountain effect



$$\Delta T \quad \curvearrowright \quad \Delta p$$



- ▶ heating of helium inside vessel \rightarrow ratio of ρ_n/ρ_s increases inside the vessel
- ▶ the temperature inside is higher than outside
- ▶ to equalize the system ρ_s flows through superleak (compressed powder)
- ▶ pressure rises and fountain starts to flow (and flows as long as heater is on)



d) Heat Transport

- ▶ in not too small capillaries $v_n \neq 0$
- ▶ even in equilibrium ($\Delta p = \rho S \Delta T$) there is a constant flow of ϱ_n from the warm end to the cold end and ϱ_s in the opposite direction by “convection”

$$\left. \begin{array}{l} \varrho_n \longrightarrow \text{cold end} \\ \varrho_s \longrightarrow \text{warm end} \end{array} \right\} \text{entropy transport} \triangleq \text{heat transport}$$

heat transport maximum at 1.8 K where $\varrho_n \approx \varrho_s$

- ▶ limited only by the mobility of ϱ_n and therefore η_n
- ▶ viscos mass flow of ϱ_n :

volume rate $\dot{V}_n = \frac{\beta}{\eta_n} \frac{\Delta p}{L}$

(*)

$$\begin{array}{l} \beta \propto r^4 \quad \text{for capillaries} \\ \beta \propto d^3 \quad \text{for slits} \end{array}$$

- ▶ entropy flow $\dot{V}_n \varrho S$ \longrightarrow heat flow $\dot{Q} = T \dot{V}_n \varrho S$ (**)

$$\delta Q = T \delta S$$



(*) insert in (**) and London equation ($\Delta p = \rho S \Delta T$)

$$\dot{Q} = \frac{\beta T (\rho S)^2}{\eta_n L} \Delta T$$

linear regime

experimental results:

$$\dot{Q} \propto \beta \propto d^3 \quad (\text{as expected})$$

$$\dot{Q} \text{ rises with } T \quad (\text{as expected})$$

heat flow $\log \dot{Q}/\Delta T$ vs $\log d$

